Chemometrically Assisted RP-HPLC Method Development for Efficient Separation of Ivabradine and its Eleven Impurities

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The aim of this study was to develop a novel reversed-phase high-performance liquid chromatography (RP-HPLC) method for efficient separation of ivabradine and its 11 impurities. Similar polarity of impurities in the sample mixture made method optimization challenging and accomplishable only when different chemometric tools, such as principal component analysis (PCA), Box-Behnken design (BBD), and desirability function as a multicriteria approach, were employed. The presence of 3 positional isomers (impurities III, V, and VI), keto-enol tautomerism of impurity VII, and diastereoisomers of impurity X made separation of this complex mixture even more challenging. Chromatographic retention parameters obtained with the mobile phase consisting of 30 mM phosphate buffer and acetonitrile (80:20, v/v) on four different RP-HPLC columns at varying pH values (3.0, 4.0, and 5.0) were subjected to the PCA analysis to select the column with the most appropriate selectivity. Then the column temperature, pH of the aqueous component of mobile phase, phosphate buffer molarity and the organic solvent content in the mobile phase were estimated employing BBD. Valid and reliable mathematical models towards resolution of twelve critical peak pairs were obtained. After determination of the desirability making criteria for all responses, desirability functions were established and used in optimization. The proposed optimal chromatographic conditions included the Zorbax Eclipse Plus C18 chromatographic column (100 × 4.6 mm, 3.5 µm), the column temperature of 34 °C, the mobile phase flow rate of 1.6 mL min⁻¹ and the UV detection at 220 nm. The mobile phase consisted of the 28 mM phosphate buffer at pH 6.0 and acetonitrile (85:15, v/v). Separation of one pair of positional isomers was not achieved, so methanol was added to the organic part of mobile phase in small increments with the optimal ratio of methanol to acetonitrile 59:41, v/v. The overall organic component of the mobile phase also increased to 18%, accelerating the chromatographic analysis.

Keywords: Ivabradine, principal component analysis, Box-Behnken design, isocratic elution RP-HPLC, diastereoisomers

Introduction

Ivabradine is chemically 3-(3-{[((7S)-3,4-dimethoxybicyclo[4.2.0]octa-1,3,5-trien-7-yl)methyl] methylamino}propyl)-1,3,4,5-tetrahydro-7,8-dimethoxy-2H-3-benzazepin-2-one hydrochloride (Figure 1). It is a novel heart beats lowering agent, with a demonstrated efficacy in treatment of chronic stable angina pectoris and myocardial ischemia with an optimal tolerability profile, because of its selective interaction with pacemaker channels [1]. The mechanism of action of ivabradine is based on reduction of the rate of pacemaker activity in the sinoatrial node by selective inhibition of the f-current (If). The named current is involved in generating an early phase of spontaneous diastolic depolarization in the pacemaker cells, enabling reduced frequency of the action potential initiation and the lower heart rate [2–4].

One of the potential synthesis pathways of ivabradine is reductive coupling of the reduced form of the derivative azepane ((7,8-dimethoxy-l,3-dihydro-2H-3-benzazepine-2-one-3-yl)-2-(1,2-dioxolan-2yl)ethane) and butamine hydrochloride (impurity I). Butamine hydrochloride along with impurities II, III, IV, V, VI, VII, VIII, and IX is recognized as impurity related to the synthesis pathway, but also as the degradation impurity. On the contrary, impurities X and XI are defined only as the potential degradation products of ivabradine. Chemical structures of all the investigated impurities are shown in Figure 1.

During the literature survey, a few analytical and bioanalytical methods for determination of ivabradine were found. Papers dealing with biological samples mostly dealt with the high-performance liquid chromatography (HPLC) and the ultra-high performance liquid chromatography (UHPLC) methods using the different detection techniques, in order to determine ivabradine and its low concentrated metabolites in urine and plasma [5-9]. Furthermore, a limited number of studies were devoted to the development of analytical methods capable of determination of ivabradine, its impurities, and/or the degradation products. Namely, only two papers dealing with optimization of the stability-indicating high-performance thin-layer chromatographic method (HPTLC), reversed-phase high-performance liquid chromatographic method (RP-HPLC), and spectrophotometric method for the separation of ivabradine and its potential degradation products formed under acidic and basic conditions were reported [10, 11]. However, no comprehensive evaluation of ivabradine's stability or assessment of the efficiency of the method separation efficiency regarding all the degradation products was provided. Nevertheless, the stress degradation was conducted in one study and used for stability estimation and determination of ivabradine's degradation pathway. Its sensitivity to acidic and basic

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Separation of Ivabradine and its Eleven Impurities



Figure 1. Chemical structures of ivabradine and its impurities and the degradation products

degradation was confirmed, together with degradation pathway dependence on the influence of hydrochloric or sulfuric acid [12]. The gradient elution HPLC method was proposed for determination of ivabradine and its 5 potential degradation products. Therefore, on the basis of a limited number of the reported methods along with the fact that present pharmacopeia does not contain a monograph of ivabradine, a comprehensive method that could enable retention evaluation of ivabradine along with its impurities, and the degradation products is urgent in this field. Furthermore, due to the different synthesis pathways, there are numbers of different impurities possibly appearing in ivabradine, whose physicochemical characterization and relation to the HPLC retention are required. Therefore, in this paper, evaluation of retention and the isocratic elution HPLC method development was studied. Separation of the proposed complex mixture was challenging, if we consider similar polarities of ivabradine and its degradation products together with the very similar physicochemical properties of the three positional isomers (impurities III, V, and VI). Through a thorough evaluation of the impurities' structures, it was noticed that keto-enol tautomerism can be expected, when dealing with impurity VII. Furthermore, impurity X represents N-oxide, a substance with 2 chiral centers. Having 2 chiral centers pointed out that formation of two diastereoisomers can occur. Diasteroisomers, unlike enantiomers, exhibit different physicochemical characteristics enabling their separation on the analytical HPLC columns using a standard mixture of the organic solvent and water as the mobile phase.

Thus, in order to obtain an efficient separation of this complex analytical mixture, the chemometric approach was applied at different stages of method development, and it included principal component analysis (PCA) for the selection of the columns, the Box–Behnken design (BBD), and the desirability function for method optimization.

Materials and Methods

Chemicals. Standard samples of ivabradine hydrochloride and its 11 impurities were kindly donated by Les Laboratoires Servier (Paris, France). Potassium hydroxide (Actavis d.o.o., Leskovac, Serbia), potassium dihydrogen phosphate (J.T. Baker, Deventer, Holland), and *ortho*-phosphoric acid 85% (Merck, Darmstadt, Germany) were of analytical grade. The HPLC-grade acetonitrile (Merck, Darmstadt, Germany) and methanol (J.T. Baker B.V., Deventer, The Netherlands) were used for the analysis. Deionized water was produced using a water purification system Simplicity 185 from Millipore (Billerica, MA, USA) at 18.2 MΩ cm resistivity.

Chromatographic Conditions and Equipment. Chromatographic analysis was performed with use of an Agilent Technologies (Palo Alto, CA, USA) HP 1200 chromatograph equipped with an on-line degasser, a binary pump, a column oven, a diode array detector, and a Rheodyne 20- μ L loop injector. Data were acquired by means of the HP ChemStation software. Chromatographic separation was performed on several chromatographic columns: Zorbax Eclipse XDB Phenyl (4.6 × 250 mm, 5 μ m) column (Agilent Technologies, Santa Clara, CA, USA), Zorbax Eclipse plus C18 (4.6 × 250 mm, 5 μ m) column (Agilent Technologies, Santa Clara, CA, USA), Zorbax Eclipse plus C8 (4.6 × 250 mm, 5 μ m) column (Agilent Technologies, Santa Clara, CA, USA), and Synergy 4u Polar-RP 80A (4.6 × 250 mm, 4 μ m) column (Phenomenex, Torrance, CA, USA).

Final separation was achieved with the Zorbax Eclipse plus C18 column (4.6×250 mm, 5 µm) termostatted at 34 °C. The analyses were carried out in the isocratic elution mode with mobile phase A, consisting of the 28 mM potassium phosphate buffer at pH 6 adjusted with *ortho*-phosphoric acid, and mobile phase B, consisting of the acetonitrile–methanol mixture (41:59, ν/ν). The A/B ratio was 82:18, ν/ν . The flow rate of the mobile phase was set to 1.6 mL/min. The detection wavelength was 220 nm.

Preparation of Mobile Phase and Standard Solutions. Stock solutions of ivabradine and the investigated impurities were prepared by dissolving an appropriate amount of standard substance in methanol, to obtain a final concentration of 100 μ g/mL for each compound. Due to the known photosensitivity of ivabradine, all solutions were protected from daylight and stored in amber glass vials within a temperature range from 2 to 8 °C.

Working samples were prepared by dissolving a proper amount of the stock solutions of ivabradine and its impurities in the mobile phase composed of A (potassium dihydrogen phosphate) and B (acetonitrile–methanol, 41:59, ν/ν) in a ratio of 81:18 (ν/ν), to obtain final concentration of 200 µg mL⁻¹ for ivabradine hydrochloride and 4 µg mL⁻¹ for each individual impurity.

The content of acetonitrile in the mobile phase (15-20%, v/v), the phosphate buffer concentration (20-40 Mm), the pH value of the aqueous phase (4-6), and the column temperature (30-40 °C) varied according to the experimental plan defined by the Box–Behnken design. The pH value of the aqueous phase was adjusted by addition of *ortho*-phosphoric acid to obtain pH 6. Further, the ratio of acetonitrile to methanol (41:59, v/v) was adjusted using the one-factor-at-a-time approach (OFAT). Portions of the mobile phase were prepared in the amounts sufficient for daily use to ensure their stability. The mobile phase was filtered through a nylon membrane filter with a 0.45-µm pore size (Agilent Technologies, Santa Clara, USA) and degassed in an ultrasonic bath prior to use.

Software. The Design Expert 11.0.0. (Modeling and Design) 10.1 v. program (Stat-Ease[®], Minneapolis, Minnesota) was used to obtain the plan of experiments and for statistical analysis of the obtained results. PCA was performed employing Statistica 13.5 (TIBCO software, CA, USA) [13, 14].

PCA Analysis. PCA is a reliable and commonly used multivariate statistical procedure converting a set of possibly correlated variables into a set of linearly uncorrelated variables called principal components (PCs). The number of PCs is lower than or equal to the number of the original variables [15–20]. Through a few PCs only, variability in the data set is assessed. Vectors recognized as eigenvectors of the matrix are used to define each PC. Variance along the vector is an eigenvalue, and it corresponds with the percentage of variance modeled by the corresponding PC. The maximum variance of the data is usually covered with the first PC, while the total variance is the sum of the variances of the original variables. To visualize the relationship between the objects and variables, the score and loading plots are constructed.

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Column	ЬH	IX–II	V-III	V-VI	IV-III	Ivabradine-IX	Ivabradine-VII	Ivabradine-IV	Ivabradine-X_1	IIV-XI	IX-X_1	IX-X_2	IX-IV	IV-VIII	IV-X_1	IV-X_2	VIII-X_1	VIII-X_2
adra suits	ю	1.71	0.00	0.00	0.00	0.00	1.16	1.16	1.16	1.16	1.16	3.71	1.16	0.00	0.00	1.14	0.00	1.14
	4	4.91	0.00	0.00	0.00	0.00	2.44	0.00	6.54	2.44	6.54	9.65	0.00	2.44	6.54	9.65	1.52	5.76
riiciiyi	S	6.25	0.00	0.00	0.00	0.00	0.00	0.00	7.06	0.00	7.06	13.32	0.00	0.00	7.06	13.32	7.06	13.32
Jolineo Dlue	т	0.00	1.52	0.00	1.52	4.72	0.00	4.72	1.63	4.72	1.45	0.00	0.00	4.72	1.45	0.00	1.63	4.72
cupse ruus	4	0.00	1.39	0.00	1.39	5.15	0.00	5.15	1.42	5.15	1.44	0.00	0.00	5.15	1.44	0.00	1.42	5.15
010	S	1.39	0.99	0.00	0.99	5.53	1.77	1.77	0.00	0.98	5.53	5.53	0.98	0.00	1.77	1.77	1.77	1.77
Joliano Dluc	т	0.00	1.27	0.00	1.27	1.63	1.63	5.08	1.63	0.00	0.00	1.11	1.11	1.11	1.11	0.00	0.00	1.11
actipse rius	4	0.00	1.05	0.00	1.05	1.59	1.59	5.12	5.12	0.00	1.02	5.12	1.02	1.02	0.00	1.67	1.02	5.12
0)	S	1.39	0.00	0.00	0.00	1.13	1.13	1.13	3.27	0.00	1.13	1.13	0.00	0.00	1.13	1.13	1.13	1.13
Concerned Arr	б	0.87	1.52	0.00	1.52	0.00	6.82	5.14	2.12	6.82	2.12	6.82	5.14	1.25	0.77	1.25	3.24	0.00
oyneigy 4u Dolor: D D 00 A	4	1.28	1.30	0.00	1.30	0.00	5.68	1.71	0.00	5.68	0.00	1.71	1.71	1.73	1.71	0.00	5.68	1.73
LUIAI-INF OUA	5	2.48	1.19	0.00	1.19	0.00	6.35	1.44	10.64	6.35	10.64	4.88	1.44	2.31	13.93	11.43	19.08	16.35



Figure 2. Score plot of the first two PC vectors

Response Surface and Multivariate Response Methodology. When only a few responses are being analyzed, the optimal region is easy to be located by mathematical equations and the 3D diagrams [21]. On the contrary, when several responses are to be optimized simultaneously, the multicriteria decision making approach (MCDM) is recommended. This approach allows identification of the best solution in the most efficient way from creation a local optimal solution to a group of different objectives. Each objective may contribute in a positive or a negative way to the final solution [22]. The path of the steepest ascent, the desirability function, and the mathematical programming are different approaches implied with MCDM. The path of the steepest ascent is applicable to the linear models only. As linear models are not usually related to the response surface methodology (RSM), this approach has not been applied. Further, when dealing with the systems where only one response could be marked as the most important, a mathematical programming approach can be taken.

Since separation of complex mixtures could not be accomplished towards only one response, this approach was not suitable. Consequently, the desirability functions applicable to both linear and non-linear models and with optimization capability towards an unlimited number of responses were selected. These functions are based on the idea that a quality of the process that has multiple quality characteristics, with one of them outside of some "desired" limits, is completely unacceptable. For each response, values of the desirability function can appear between 0 and 1, where 0 represents completely undesired values of response, and 1 represents a completely desirable or ideal response value [23]. Before starting the optimization process, the priorities and desires for each response must be defined. These priorities are defined through the responses' bounds, goals, and weights (wti). For different transformation could be one-sided goals, (maximization and minimization) and two-sided (target value and in range). The weights emphasize a goal, an upper or lower



Figure 3. Loading plot of the first two PC vectors

Table 2. Investigated variables and their domains

Investigated variable	Defined	l level of v	ariables
	-1 level	0 level	+1 level
pH of water phase	4	5	6
Column temperature (°C)	30	35	40
Acetonitrile (%)	15	17.50	20
Concentration of phosphate buffer (mM)	20	30	40

bounds, or a target value. With wt_i of 1, the desirability function (d_i) can vary from 0 to 1 in a linear way, while approaching a desired value. The weights higher than 1 stronger emphasize the goal, whereas the weights lower than 1 give less emphasis to the goal, and in both cases, d_i varies in a non-linear way [21].

The desirability values are calculated using Eq. (1), when the goal is maximization:

$$d_i = \left[\frac{Y_i - \text{Low}_i}{\text{High}_i - \text{Low}_i}\right]^{\text{wt}_i} \quad \text{Low}_i < Y_i < \text{High}_i \qquad (1)$$

where Y_i is the predicted response using the fitted model, and the highest and the lowest values are obtained for the response, respectively, and wt_i is the weight.

The desirability values are calculated using Eq. (2), when the goal is minimization:

$$d_i = \left[\frac{\text{High}_i - Y_i}{\text{High}_i - \text{Low}_i}\right]^{\text{wt}_i}$$
(2)

Eq. (3) is used, when the goal is a target value, where the desirability ramps are formed similar to a maximum on the way up, and a minimum on the way down:

$$d_{i} = 0, \qquad za \qquad Y_{i} < \text{Low}_{i}$$

$$d_{i} = \left(\frac{Y_{i} - \text{Low}_{i}}{\text{target}_{i} - \text{Low}_{i}}\right)^{\text{wt}_{i}}, \qquad za \qquad \text{Low}_{i} < Y_{i} < \text{target}_{i}$$

$$d_{i} = \left(\frac{Y_{i} - \text{High}_{i}}{\text{High}_{i} - \text{target}_{i}}\right)^{\text{wt}_{j}}, \qquad za \qquad t_{i} < Y_{i} < u_{i}$$

$$d_{i} = 0, \qquad za \qquad Y_{i} > u_{i}$$
(3)

where $target_i$ is the target value.

For a goal within a range, Eqs. (4) and (5) are used:

$$d_i = 0, \text{ for } Y_i = \text{Low}_i \tag{4}$$

J. Tomić et al.

$$d_i = 1, \text{ for Low}_i < Y_i < \text{High}_i \tag{5}$$

When individual desirability functions d_i are obtained, the overall desirability function (D) is further estimated. The D value can range from 0 for the totally undesirable responses to 1, when all responses are desirable. In this paper, the Derringer desirability function is used, where the D function is calculated, using Eq. (6):

$$D = \left(d_1^{rt_1} d_2^{rt_2}, \dots, d_I^{rt_l}\right)^1 / \sum^{rt_i}$$
(6)

where r represents the importance of each response, and it gets the values from 1 to 5. Value 1 is assigned to the responses that are of lower importance, and the higher the value of r, the greater is the importance of the response.

Table 3. The Box–Behnken design plan of experiments for four variables and resolutions of the critical peak pairs as the investigated responses (pH = value of water phase; T = column temperature (°C); ACN – percentage of acetonitrile as an organic mobile phase modifier (%), Buffer = concentration of the phosphate buffer in aqueous mobile phase (mM))

Inves	stigated	d variabl	es						Re	esponses					
with	in their	domain	S												
рН	Т	ACN	Buffer	Rs	Rs	Rs	Rs	Rs	Rs	Rs	Rs	Rs	Rs	Rs	Rs
				(I/XI)	(III/V)	(V/VI)	(III/VI)	(IVB/X_1)	(IVB/X_2)	(IX/VIII)	(IX/X_2)	(IX/IV)	(IV/VIII)	(IV/X_1)	(IV/X_2)
4	30	17.5	30	1.46	0.74	0.00	1.19	4.82	4.14	0.00	1.52	1.52	1.52	0.42	0.00
6	30	17.5	30	12.06	0.63	1.83	0.88	5.90	5.14	1.26	14.89	5.61	4.21	5.90	5.14
4	40	17.5	30	1.56	1.40	0.00	1.4	3.55	3.21	1.68	0.00	0.00	-0.11	0.95	0.00
6	40	17.5	30	15.31	1.21	2.25	1.18	9.55	7.93	0.00	14.58	7.58	7.58	7.37	5.92
5	35	15.0	20	7.77	1.11	1.11	0.32	2.17	3.12	0.00	1.10	0.00	1.01	1.97	1.10
5	35	20.0	20	2.20	1.28	0.00	1.28	0.00	0.00	1.26	3.62	1.26	0.00	2.29	2.29
5	35	15.0	40	6.05	0.54	0.00	0.00	1.97	3.07	0.00	1.13	1.52	1.52	3.69	4.69
5	35	20.0	40	1.26	0.75	0.00	0.00	0.91	0.00	0.00	1.87	0.00	0.00	2.92	1.87
4	35	17.5	20	1.98	1.35	0.20	1.35	4.93	5.79	1.22	2.21	2.21	2.57	0.95	0.00
6	35	17.5	20	15.42	1.10	2.56	1.11	6.74	7.03	0.29	13.3	7.10	7.10	6.39	5.56
4	35	17.5	40	1.29	0.76	0.00	0.60	2.10	3.73	0.00	1.61	1.61	1.61	1.61	0.00
6	35	17.5	40	12.92	0.62	1.88	0.48	7.31	6.50	0.00	12.30	7.65	7.65	8.71	7.55
5	30	15.0	30	6.80	0.58	0.39	0.89	1.94	2.77	0.74	1.85	3.25	1.61	1.52	1.06
5	40	15.0	30	7.70	1.26	0.40	0.84	2.47	3.37	0.00	0.54	0.00	0.00	1.19	2.73
5	30	20.0	30	1.19	0.76	0.00	1.04	0.00	0.00	0.00	1.75	-1.12	-1.11	1.75	1.75
5	40	20.0	30	2.21	1.30	0.00	1.33	0.95	0.00	1.45	4.08	1.45	0.00	3.22	2.06
4	35	15.0	30	4.38	0.99	0.00	0.00	4.40	6.46	0.00	0.51	1.62	1.62	0.00	1.37
6	35	15.0	30	22.10	0.76	2.93	2.03	7.54	7.78	1.21	15.47	8.42	9.01	6.79	5.85
4	35	20.0	30	0.01	1.12	0.00	2.41	1.76	3.13	1.71	0.00	1.08	1.36	1.36	0.00
6	35	20.0	30	7.51	1.19	1.19	0.00	6.51	5.35	0.00	11.85	5.00	5.00	4.62	4.62
5	30	17.5	20	3.70	0.70	0.69	0.96	0.00	1.38	0.00	2.47	0.00	0.00	2.03	2.47
5	40	17.5	20	5.66	1.57	0.71	1.08	1.31	1.24	1.43	4.19	1.43	0.00	2.75	2.75
5	30	17.5	40	2.48	0.35	0.00	0.00	0.00	1.13	0.00	2.02	0.93	0.00	2.62	2.02
5	40	17.5	40	2.45	0.98	0.00	0.18	0.00	0.00	0.00	1.62	0.00	0.00	3.14	1.62
5	35	17.5	30	6.75	1.05	0.10	0.45	0.55	0.36	0.01	2.59	0.53	0.01	3.59	2.60
5	35	17.5	30	2.99	0.99	0.01	0.40	1.09	0.00	0.21	3.42	0.12	0.15	3.00	3.02
5	35	17.5	30	3.76	1.20	0.20	0.38	0.00	0.71	0.00	2.17	0.21	0.02	2.83	2.17

The greatest benefit of the desirability functions is reducing the multicriteria problem to a single criterion problem that can be optimized in a simpler way [21, 24–26].

Results and Discussion

Generally, separation in RP-HPLC strongly depends on the column type and selectivity, physicochemical properties of the investigated analytes, and chromatographic conditions, and for this reason, the first step in the separation of ivabradine and its 11 impurities was to select an appropriate column. For an efficient selection of the proper RP-HPLC column, PCA was employed. At the next step, the experimental domains of the most influential chromatographic parameters were determined and optimized using BBD as one of the response surface designs. The obtained mathematical equations were applied to the Derringer's desirability function, while resolutions of all critical peak pairs were marked as system's responses. When the optimal separation conditions were determined, an additional optimization by the one-factor-at-a-time (OFAT) approach was performed to adjust the ratio of acetonitrile and methanol in the mobile phase, since the results of the desirability function approach indicated that this was the only variable left to be optimized.

In the course of the preliminary experiments, the keto–enol tautomers of impurity VII and the diastereoisomers of impurity X were separated under some of the examined experimental conditions. Further, in order to distinguish the isomers, the keto–enol tautomers were labeled as VII_1 and VII_2, respectively, while the diastereoisomers were labeled as X_1 and X_2 .

Classification of RP-HPLC Columns towards Resolution of Ivabradine and its Eleven Impurities. PCA is taking 4 different RP-HPLC columns at varying mobile phase buffer pH values (3.0, 4.0, and 5.0) into the account. The subject matter of PCA is resolution (Rs) between the closely eluting components. Different elution order of the investigated analytes was observed under the different buffer pH values, and the resolution data used in PCA is shown in Table 1. None of the examined columns independent of the employed buffer pH values allow separation of impurities V and VI. Furthermore, there were several critical peak pairs, whose separation was hardly achieved on the investigated columns. The following peak pairs were found as critical: impurity III and impurity V, impurity III and impurity VI, ivabradine and impurity IX, ivabradine and impurity VIII, ivabradine and impurity IV, impurity VIII and impurity IV, impurity IX and impurity IV, and impurity IX and impurity VIII.

The analysis showed that 94.03% total variation could be explained with 5 components, each of them explaining 45.43, 25.37, 14.19, 4.87, and 4.17%, respectively. The first 2 PCs accounting for 70.8% of cumulative variation were retained for further analysis.

To properly analyze the results, the score (Figure 2) and loading plots (Figure 3) were obtained. The score plot shows location of the objects in the multivariate space of the first 2 PC score vectors, while the loading plot visualizes the pattern of correlation between the variables, showing the influence of the variables on the model, as well as their mutual correlation. The chromatographic parameters which are more distant from the axis origin have a greater impact on positioning of the RP-HPLC columns of similar characteristics.

When analyzing the obtained score and loading plots, there is a rule stating that the samples in the right part of the score plot have high values for the variables placed in the right part of the loading plot. In addition, the samples in the left part of the score plots, regardless of their bottom or top placement, have high values of the variables placed in the left part of the Table 4. Coefficients of mathematical models for the investigated response, their corresponding p-values and coefficients of determination

Response	Rs_1	<i>p</i> -value	Rs_2	<i>p</i> -value	R_{S_3}	<i>p</i> -value	Rs_4	<i>p</i> -value	R_{S_5}	o-value	Rs_6	<i>p</i> -value	Rs_7	<i>p</i> -value	R_{S_8}	<i>p</i> -value	Rs ₉ 1	o-value	Rs_{10}	<i>p</i> -value	Rs_{11}	<i>p</i> -value	Rs_{12}	<i>p</i> -value
Model coefficients	1																							
Intercept	+2.890	$< 10^{-4}$	1.08	$< 10^{-4}$	0.103	$< 10^{-4}$	0.410	$< 10^{-4}$	0.547	$< 10^{-4}$	0.357	$< 10^{-4}$	0.075	$< 10^{-4}$	2.73	$< 10^{-4}$	0.288	$< 10^{-4}$	0.062	$< 10^{-4}$	3.14	$< 10^{-4}$	2.60	$< 10^{-4}$
	-16.95	0.001	-0.071	0.005	1.04	0.001	-0.105	0.018	1.830	$< 10^{-4}$	1.11	$< 10^{-4}$	-0.154	0.006	6.38	$< 10^{-4}$	2.78	< 10 ⁻⁴	2.66	$< 10^{-4}$	2.87	$< 10^{-4}$	2.77	$< 10^{-4}$
В	+0.956	0.136	0.330	0.001	0.038	0.342	0.088	0.043	0.431	0.049	0.099	0.541	0.213	0.001	0.042	0.905	0.022	0.894	0.103	0.419	0.365	0.039	0.220	0.404
С	+1.561	0.001	0.096	0.001	-0.303	0.001	0.165	0.001	-0.863	0.001	-1.51	$< 10^{-4}$	0.206	0.001	0.214	0.550	-0.595	0.003	-0.793	$< 10^{-4}$	0.083	0.606	-0.351	0.189
D	+0.600	0.042	-0.258	0.001	-0.282	0.001	-0.403	0.001	-0.238	0.248	-0.344	0.049	-0.350	$< 10^{-4}$	-0.528	0.155	-0.024	0.886	0.008	0.947	0.526	0.006	0.298	0.261
AB	+0.157	0.250	-0.019	0.595	0.105	0.137	0.022	0.742	1.230	0.003	0.930	0.005	-0.735	$< 10^{-4}$	0.302	0.625	0.872	0.009	1.25	$< 10^{-4}$	0.235	0.406	I	T
AC	-1.021	0.002	0.076	0.054	-0.435	0.001	-1.110	0.001	0.402	0.260	0.225	0.426	-0.730	$< 10^{-4}$	-0.776	0.222	-0.720	0.026	-0.937	0.001 -	-0.882	0.007	I	I
AD	-0.045	0.500	0.027	0.459	-0.121	0.091	0.031	0.647	0.850	0.028	0.382	0.186	0.232	0.014	-0.100	0.871	0.287	0.329	0.377	0.104	0.415	0.154	I	I
BC	+0.002	0.964	-0.033	0.368	-0.002	0.980	0.085	0.228	0.105	0.763	-0.150	0.593	0.547	$< 10^{-4}$	0.910	0.157	1.46	0.002	0.680	0.008	0.450	0.125	I	I
BD	-0.010	0.460	-0.059	0.125	-0.006	0.926	0.015	0.824	-0.327	0.355	-0.247	0.382	-0.357	0.001	-0.530	0.396	-0.591	0.059	0.001	1.000 -	-0.050	0.858	I	I
CD	+0.008	0.770	0.011	0.758	0.277	0.001	-0.240	0.005	0.277	0.431	0.012	0.964	-0.315	0.002	-0.445	0.474	-0.695	0.030	-0.127	0.563 -	-0.272	0.337	I	I
A^2	+3.688	0.001	-0.015	0.635	0.880	0.001	0.517	0.001	4.660	0.001	4.67	$< 10^{-4}$	0.374	0.002	4.90	$< 10^{-4}$	3.61	$< 10^{-4}$	3.94	$< 10^{-4}$	0.974	0.001	I	I
B^2	-0.019	0.403	-0.066	0.055	0.060	0.315	0.310	0.002	0.337	0.275	0.182	0.455	0.272	0.002	0.055	0.918	0.016	0.950	-0.491	0.021	-0.552	0.037	I	I
C^2	+0.054	0.563	-0.044	0.179	0.028	0.631	0.206	0.004	0.353	0.254	0.775	0.007	0.248	0.004	-0.662	0.229	0.244	0.338	0.299	0.134 -	-0.745	0.008	I	I
D^2	-0.004	0.478	-0.110	0.004	0.170	0.012	-0.141	0.031	-0.045	0.882	0.517	0.049	-0.023	0.753	-0.203	0.703	I	0.130	0.479	0.024	0.224	0.362	I	I
Lack of Fit	I	0.914	Ι	0.917	I	0.364	Ι	0.059	I	0.431	I	0.306	I	0.384	Ι	0.212	Ι	0.114	I	0.028	I	0.373	I	0.187
R^2	I	0.973	I	0.975	I	0.990	I	0.979	I	0.973	I	0.980	I	0.971	I	0.975	I	0.981	I	0.990	I	0.972	I	0.844
$\operatorname{Adj} R^2$	I	0.942	Ι	0.946	I	0.978	Ι	0.955	I	0.942	I	0.958	I	0.937	Ι	0.945	I	0.958	I	0.977	I	0.939	I	0.815
Pred R^2	I	0.883	Ι	0.891	Ι	0.946	I	0.880	I	0.855	I	0.892	I	0.843	Ι	0.859	I	0.891	I	0.940	I	0.848	I	0.755
A, pH va	ue: B, co	lumn ten	perature;	C, acetor	nitrile; D), phospha	ate buffer.																	
Rei-Rs (Imr	urity I an	d XD: Re		purity III	and V):	Res-Rs (I	mpurity V	V and VI)	Rea-Rs	(Impurity	' III and	VD: Res-	Rs (Imni	urity IVB	and X-1)	: Rec-Rs	Impurity	IVB and	X-2): R	er-Rs (Im	nurity L	X and VII	D: Reo-R	<i>.</i>
	C A Pro	. D D.		I V and	d VI	D of Ger	TV/	UIII/I Pos	D D D	(Immerity	Luc IVI .	0 . (1 A	D 2 O	11/1	III/A Pere		from Joo						00 (/-	2
(Impurity 12	and A-2	1; KS9-KS	Timpdum	y LA anu	$1V$; K_{S1}	0-KS (ump	ourity 1V a	ind vill;	KS11-IVS	(Impurity)	/ IV anu	A-1), KS	2-KS (III	ipurity 1v	and v III									



Desirability = 1.000Solution 6 out of 23

Figure 4. Bar plots for the proposed optimal chromatographic conditions and the resolution values for all twelve critical peak pairs

loading plot. The score plot (Figure 2) shows that the RP-HPLC columns are classified into 4 groups. The type of the RP-HPLC column together with the buffer pH value under investigation is arranged close to each other on the basis of similar characteristics in terms of the critical pair resolution factors.

The Eclipse Phenyl column at the buffer pH values of 4 and 5 is placed in the lower right part of the score plot, enabling resolution of the following pairs: impurity II-impurity XI and impurity IX-impurity X 2. However, these pairs were not considered as critical for the analysis. On the other hand, the Synergi Polar RP column at buffer pH 5 appears in the upper right part of the score plot providing high Rs values for the following pairs: ivabradine-impurity VIII, impurity IVimpurity X₁, impurity VIII-impurity X₁, impurity IV-impurity X 2, impurity IX-impurity X 1, ivabradine-impurity X 1, and impurity VIII-impurity X 2, out of which only ivabradine-impurity VIII was considered as a critical pair. Further, in the lower left quadrant of the score plot, the Eclipse Phenyl column at pH 3, the Eclipse Plus C18 column at pH 5, and the Eclipse Plus C8 column at pH 3, 4, and 5 are placed, enabling adequate separation of ivabradine and impurity IX. The Eclipse Plus C18 column at pH 3 and 4, as well as the Synergi Polar RP column at pH 3 and 4 placed in the upper left quadrant of the score plot provided the high Rs factor values with the following critical pairs: ivabradine-impurity IV, impurity III-impurity VI, impurity III-impurity V, impurity IX-impurity VIII, impurity IX-impurity IV, and impurity IV-impurity VIII. To sum up, the decision about a proper column was based on the high Rs values for the aforementioned critical pairs. Columns placed in the upper left quadrant managed to resolve a vast majority of the critical pairs. Eventually, from among these columns, the Eclipse Plus C18 column was selected, since under the different buffer pH values, it enabled separation of ivabradine and impurity IX as well.

BBD and Desirability Function in Optimization of Chromatographic Parameters. According to preliminary experiments and the results of PCA, the significant chromatographic variables and their domains were established and presented in Table 2.

From a considered list of the organic modifiers, acetonitrile was chosen as one of the most efficient organic modifiers used in RP-HPLC. Potassium phosphate buffer (KH₂PO₄) was used as the aqueous component of the mobile phase, in order to additionally improve peak symmetries and to adjust the pH values within the defined domains. The appropriate pH value and the molarity of the buffer, as well as its influence on the retention, were estimated with the aid of BBD. The PCA responses provided an insight into the retention behavior of the analytes and suggested widening of the pH range from 4 to 6. The last variable that could influence not only the retention but also the separation was the column temperature, so it was also included in the BBD.

Though the analytes are of similar polarity and the mixture includes three positional isomers, keto–enol tautomers and 2 diastereoisomers, it was decided to check a possibility of separation in the isocratic elution mode. This decision was quite reasonable bearing in mind simpler retention mechanisms in the isocratic elution mode, reproducible results, and no ghost peaks.

BBD was conducted according to the experimental plan presented in Table 3. The selected responses were resolutions between the adjacent peaks, taking into consideration all critical peak pairs. Those were resolutions between impurities I and XI, III and V, V and VI, III and VI, IX and VIII, IX and X_2, IX and IV, IV and VIII, IV and X_1, and IV and X_2, as well as resolutions between ivabradine and impurities X_1 and X_2 . Resolutions obtained according to experimental plan for



Figure 5. The 3D response surface plots of the overall desirability function (D) for optimization of pH and the column temperature (A), pH and acetonitrile (B), acetonitrile and the phosphate buffer molarity (C), and pH and the phosphate buffer molarity towards the proposed goals

all 12 critical peak pairs are presented in Table 3. For 11 responses, the software proposed the quadratic mathematical models and, only for Rs between impurities IV and VIII, the linear mathematical model. Coefficients of these mathematical models along with their corresponding p-values are presented in Table 4. The larger the absolute value of the coefficient, the higher the influence of the variable towards the response. If the coefficients are positive, an increase in the variable influences the increase in the response value and vice versa. On the contrary, if the coefficients are negative, an increase in the variable influences the decrease in the response value. Nevertheless, statistical significance of the variables is estimated using the corresponding *p*-values for all coefficients. Table 4 shows that percentage of organic modifier and pH of aqueous phase have the highest influence on all responses, while buffer concentration and column temperature appeared less influential, although statistically significant towards most responses. For that reason, all variables were taken into the account in the further optimization process. The validity of all models was confirmed by a nonsignificant lack of the fit test values and high values of the coefficient of determination. Coefficient of determination (R^2) , the adjusted R^2 , and the predicted R^2 values were above 0.885 pointing out to a good predictive ability of the models and to their ability to explain more than 88% total variance.

Models with the confirmed validity and predictive ability were used in the multicriteria optimization process. The optimization criteria included the response bounds, the aims for all responses, and the defined weights and importance. The same values of weights and importance equal to 1 were set for all the responses, since all resolutions were of the same interest and their threshold was equal to or higher than 2. The response bounds were set from the lowest to the highest values of the obtained resolutions, and the overall criteria were in the range from 2 to the highest possible value. All these criteria are presented in Figure 4. For 2 resolutions, those between impurities III and V and IX and VIII, no experimental conditions in the defined experimental range could allow an adequate separation and the resolution factor higher than 2, so that for a while, these resolutions were left out from the optimization process, and no criteria were defined for them. For all the remaining responses, the software offered 23 solutions, and from which, solution 6 was selected. Solution 6 was the only one enabling the highest resolutions for the critical peak pairs between impurities III and V, and IX and VIII. In Figure 4, the obtained resolutions for all 12 critical peak pairs are presented. The optimal chromatographic conditions included the 28 mM phosphate buffer at pH 6, 15% acetonitrile in mobile phase, and the column temperature of 34 °C. To gain a better insight into the system behavior and an adequacy of the selected optimal chromatographic conditions, the 3D plots of the



Figure 6. Contour plots that represents the influence of pH values and content of acetonitrile towards resolution of (A) impurities I and XI, (B) impurities III and V, (C) impurities V and VI, (D) impurities III and VI, (E) ivabradine and impurity X_{1} , (F) ivabradine and impurity X_{2} , (G) impurities IX and VIII, (H) impurities IX and X_{2} , (I) impurities IX and IV, (J) impurities IV and VIII, (K) impurities IV and X_{1} , (L) impurities IV and X $_{2}$

global desirability function were presented in Figure 5. Detailed assessment of the 3D response surface plot pointed out that pH 6 of aqueous component of the mobile phase and 15% acetonitrile were the only preconditions which secured the satisfactory optimization criteria. On the contrary, the molarity of the buffer could differ from 26 to 29 mM (Figures 5C and 5D), and the column temperature could differ from 32 to 34 °C (Figure 5A). In order to obtain better insight into the influence of pH values and amount of acetonitrile, as the most significant variables, contour plots of these variables towards all critical peak pears are presented in Figure 6. Contour plots indicated that bounder pH values such as 4 and 6 enabled separation of critical peak pears. Moreover, satisfactory separation of impurities III and V, and IX and VIII could



Figure 7. Representative chromatogram of ivabradine (ca. 200 μ g/mL) mixed with eleven impurities (ca. 4 μ g/mL each), obtained under the proposed chromatographic conditions using the desirability function (A), Representative chromatogram of ivabradine (ca. 200 μ g/mL) mixed with eleven impurities (ca. 4 μ g/mL each) obtained under the optimal chromatographic conditions (B)

be achieved at pH 4 with acetonitrile content in the mobile phase close to 20%. However, these chromatographic conditions are unacceptable for other critical resolutions, and consequently desirability function defined pH 4 and acetonitrile content of 20% as undesirable.

The representative chromatogram obtained under the optimal chromatographic conditions is presented in Figure 7A. According to the expectations, resolution between impurities III and V and IX and VIII did not fulfill the separation requirements, and a consecutive study was necessary. It is important to note that the criteria for Rs differ, depending on the type of the analyte investigated and the corresponding peak areas. The Rs value above 1.5 could provide the baseline separation of impurities, due to rather small and similar peak areas, while this is not the case, when separating an active substance from the impurities, since their corresponding peak areas are significantly different. A possibility of overlapping between active substance and impurity even exists in the case of perfect peaks' symmetries. Additionally, the peak tailing of active substance can lead to a significant reduction in resolution, most peak of active substance. For this reason, resolution higher than 2 and, in some cases, even 2.5 is required between the peak of active substance and the peak of impurity [27, 28]. Since separation of 2 critical peak pairs included impurities, the separation criterion was set at Rs of ca 1.5. In that respect, the pair of positional isomers (impurities III and V) remained critical, while impurities IX and VIII were satisfactorily separated with Rs of 1.31. For this reason, methanol as an organic modifier of a lower elution strength was included in the mobile phase as well. Addition of methanol to the organic component of mobile phase led to co-elution of diastereoisomers of impurity X, and the separation of diastereoisomers X₁ and X_{2} could not be achieved. This phenomenon can be related to some physicochemical properties of used organic solvents, methanol, and acetonitrile. When acetonitrile is used as a single organic modifier, its molecules form an adsorbed double layer on the surface of the stationary phase, creating a beneficial surrounding for electrostatic interactions. When methanol is added to the mobile phase, it forms a monolayer on the

notably in the case when the peak of impurity elutes after the

stationary phase surface, and different interactions are occurring [29]. As a consequence, separation of diastereoisomers is lacking, and impurity X is eluting as one peak. An appropriate ratio of acetonitrile and methanol in the organic part of mobile phase was adjusted using the OFAT approach, since only two variables towards the two responses were left. The percentage of methanol was increased in small increments (1%), while the percentage of acetonitrile was simultaneously and reciprocally decreased to retain 15% of the overall organic part of the mobile phase as defined in the optimization process. It was proven that the organic component of mobile phase must be acetonitrile-methanol in the ratio of 41:49, v/v. During this process, separation of the critical peak pairs was improved, but the retention time of the chromatographic run was also increased. Furthermore, the amount of the organic phase was decided to be 18%, in order to reduce the duration of the overall chromatographic run time. The representative chromatogram obtained under the chromatographic conditions from the second optimization is presented in Figure 7B.

With respect to all the presented and discussed data, the developed method could be labeled as suitable for the separation of ivabradine and its 11 impurities. Nevertheless, the main drawback of the proposed method is a relatively long run time. For this reason, the authors plan to direct their further work to the development of the gradient elution chromatographic method for the separation of the investigated analytes.

Conclusion

In this study, we, for the first time, presented a chemometrically supported chromatographic method for the separation of ivabradine and its 11 impurities. Based on the PCA results, the Zorbax Eclipse Plus C18 column was chosen as that with optimal selectivity. Additional optimal chromatographic conditions selected using BBD and the desirability function towards 12 critical peak pairs included the 28 mM phosphate buffer at pH = 6.0, the column temperature 34 °C, and 15% acetonitrile in the mobile phase. The mobile phase flow rate was set to 1.6 mL min⁻¹. The first assessed separation conditions did not manage to adequately resolve the positional isomers. For this reason, a small increment of methanol was added to the organic part of mobile phase, with an optimal ratio of methanol to acetonitrile equal to 59:41, v/v. The overall organic part of mobile phase was increased to 18%, in order to accelerate chromatographic analysis.

Abbreviations

RP-HPLC: reversed-phase high-performance liquid chromatography, UHPLC: ultra-high-performance liquid chromatography, HPTLC: high-performance thin-layer chromatography,

PCA: principal component analysis, PC: principal components, BBD: Box-Behnken design, OFAT: One Factor at a Time, MCDM: multicriteria decision making, RSM: response surface methodology, d_i : individual desirability functions, D: overall desirability function

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